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Description

This invention relates to coin discriminating apparatus.

Various proposals have been made for coin discriminating apparatus in which eddy currents are induced in a coin and the effect of the eddy currents on an electrical circuit are monitored.

In some arrangements a single coil is connected to an A.C. source and the effect of the eddy currents on the coil current is detected, whereas in other arrangements two coils are employed, one being connected to the A.C. source to induce eddy currents and the other to a monitoring circuit.

It has also been proposed in Patent Application GB—A—2 041 532 to monitor the decay of eddy currents produced in a coin by a pulse in a coil.

Such pulse induction methods have been used in metal detectors. US—A—3 707 672 discloses a metal detector which is designed to discriminate between different metals and different objects, in particular to identify a hand gun concealed in luggage. A transmitting coil is subjected to a train of pulses, and the rate of change of the magnetic field occurring at either the initiation or termination of the pulses is measured with a receiver coil and is compared with references to identify the metal object in terms of thickness.

The known arrangements are theoretically capable of distinguishing between certain coins, but in practice they would not provide satisfactory discrimination between coins of several different denominations, and additional non-inductive coin tests would need to be employed.

In practice it may, for example, be necessary to distinguish between British 50 pence, 10 pence, 5 pence and 2 pence coins which have been validly inserted into a coin-released mechanism, and also to distinguish bogus coins such as one pence coins, washers and slugs which should not have been inserted into the particular mechanism.

The term 'coin' used hereinafter is therefore intended to include bogus coins such as washers, and also tokens.

The present invention has resulted from our attempts to improve inductive coin testers to deal with situations in which coins of a range are to be distinguished.

One problem with the previously proposed arrangements is that usually they will not distinguish between coins of different diameters when they are made of the same material, and another problem is that they can even be confused by coins of quite different materials in certain circumstances.

We have studied these problems in arrangements in which eddy currents are induced in a coin by a pulse applied to a coil and the decay of the eddy currents is monitored, and we have realised that the problems are associated with the fact that the rate of decay of the eddy currents is dependent upon the ratio L/R where L is the inductance of the eddy current loop induced in the coin, and R is the resistance of that loop. The

ratio L/R can be the same for different denominations of coin.

For example, the ratio L/R is the same for 1976 2p coins and some worn one shilling coins dated prior to 1948, when the coins are encircled by the pulsed coil, even though the material of the coins is quite different.

A further problem which arises with inductive coin testers is that when the eddy currents are induced in the surface of a plated coin it is the resistivity of the plating which is effectively being measured, and it is necessary in some circumstances to be able to distinguish between plated and un-plated coins.

According to the invention a coin discriminating apparatus comprises coil means for inducing eddy currents in a coin, pulsing means for pulsing the coil means, and means for monitoring the decay of eddy currents in the coin, characterised in that the pulsing means is arranged to pulse successively a coil or different coils of the coil means with voltage pulses of shorter and longer durations.

A short voltage pulse, for example a pulse of 5µs, will induce eddy currents in the coin surface only, whereas a long voltage pulse, for example a pulse of 200µs, will induce eddy currents in the full thickness of a coin, and so the rate of decay of the eddy currents will depend upon the resistivity of the material of the coin surface for a short pulse, and upon that of the body of the coin for a long pulse, making it possible to distinguish plated coins. The reason is that the coil current will have built up to a higher value by the end of a long voltage pulse than for a shorter voltage pulse, and accordingly larger eddy currents in the coin will result in termination of the voltage pulse.

In order to reduce the requirements as to the dynamic range of the monitoring circuitry it is preferred that the delay between the lagging edge of the voltage pulse and the measurement of the eddy currents, by sampling the current in a receiver coil, is made longer for a long voltage pulse than for a short voltage pulse.

In one embodiment a single coil is used both as a transmitting coil and as a receiving coil, and the coil is successively pulsed with four voltage pulses of different durations. This can provide a relatively cheap arrangement, suitable for a coin validator, since there is only one coil.

It is also possible for the coil means to comprise two coils, one of which is pulsed with a long pulse, the other being pulsed at a different time with a short pulse.

In order to provide additional information, in one preferred arrangement the coil means comprises first and second transmitting coils of larger and smaller effective cross-sectional areas respectively, and the pulsing means is arranged to apply a voltage pulse to one of the transmitting coils followed by a voltage pulse to the other transmitting coil, and the monitoring means is arranged to monitor the decay of eddy currents produced in a coin by the lagging edge of the resulting current pulses in the transmitting coils

when the coin is positioned adjacent to the respective transmitting coils.

One or both of the transmitting coils may be arranged to be pulsed with said pulses of shorter and longer duration.

Preferably the projected effective cross-sectional area of the first transmitting coil onto a coin positioned adjacent to that coil by a location means is arranged to be greater than that of the face of at least most of the coins that are to be distinguished, and the location means is so arranged that the boundary of said projected area of the first transmitting coil encircles the coin when the eddy currents are induced in the coin by pulsing of the first transmitting coil, and the arrangement is such that the projected effective cross-sectional area of the second transmitting coil lies within the area of the face of at least most of the coins when the coin is positioned adjacent to the second transmitting coil by the location means and that coil is pulsed.

The first transmitting coil of larger area will induce currents in the periphery of a coin positioned adjacent to it, so that the diameter of the eddy current loop in the coin will be substantially that of the coin, and will therefore differ for coins of different diameters. However, the diameter of the eddy current loop induced in coins by the second transmitting coil of smaller area will be substantially the same for different coins.

Since the rate of decay of eddy currents is dependent upon the ratio L/R of the short circuit turn, and the inductance L is proportional to the area of the turn πr^2 , where r is the radius of the short circuit turn, and the resistance R is proportional to $p \cdot 2\pi r$, where p is the resistivity of the material of the coin through which the eddy currents flow, the rate of decay is dependent on the ratio r/p . This ratio for eddy currents induced by the first transmitting coil will vary in dependence upon both the coin diameter and resistivity, whereas for eddy currents induced by the second transmitting coil r is substantially constant so that the ratio r/p will change only for materials of different resistivities.

Thus, monitoring the rates of decay of eddy currents produced by the two transmitting coils substantially increases the chances of distinguishing between coins of various materials and diameters.

It will be appreciated that measurements on the decaying eddy currents produced by one transmitting coil should be completed before eddy currents are induced by pulsing of the other transmitting coil.

The first transmitting coil may be pulsed prior to the second transmitting coil or vice versa.

The first and second transmitting coils are preferably positioned such that the coin being tested is substantially in the same position during pulsing of the first and second transmitting coils, but if desired the transmitting coils may be placed at spaced positions along a coin path. The measurements can be made extremely

quickly so that it does not matter if the coins are moving quickly past the coils.

One or both of the transmitting coils may also act as a receiver coil responsive to the induced eddy currents and connected to the monitoring circuit, or one more independent receiver coils may be provided.

In one preferred arrangement the first and second transmitting coils are positioned together, and the first coil acts as the receiver coil both for when the first transmitting coils is pulsed and when the second transmitting coil is pulsed.

The monitoring circuit is preferably arranged to measure the magnitude of the decaying eddy currents at three predetermined times subsequent to the initiation of the eddy currents. At first sight it might appear that measurement of the coil current at only two times would be sufficient to characterise the decay curve. However, since the eddy current distribution in the coin changes with time, in particular in relation to the depth of the eddy currents in the coin, and since some coins are plated, the third measurement can help to distinguish between plated and un-plated coins. This is because two points define a unique exponential as well as a straight line. The decay is not a simple exponential due to the skin depth effect. As the eddy current loop decays the cross sectional area through which the eddy currents flow reduces. This results in the resistance and inductance of the loop increasing. However, the inductance of the loop increases faster than the resistance so the decay rate is slower than a simple exponential. This effect is more marked if the coin is thicker and is thereby used to assist in detecting coin thickness.

The receiver coil is preferably arranged to be critically damped by a suitable choice of the input resistance of the monitoring circuit to enable the measurements to be made in a minimum time.

The transmitting coils may be in the form of printed circuit spirals, possibly arranged as two concentric spirals.

Coin discriminating apparatus in accordance with the invention may be used in conjunction with a microprocessor memory circuit which is arranged to learn the various characteristics of a coin when in a learn mode the apparatus is fed with a range of coins of a given denomination. The circuit stores maximum and minimum values of the various coil voltage measurements for each denomination of coin, and then in the normal operating mode the measured coil voltages of a coin under test are compared with the stored values to identify the coin. This avoids the need for an extensive calibration procedure, and can enable the apparatus to be put into operation with different coinages without the need for specific modifications or calibration to be made.

The invention will now be further described, by way of example only, with reference to the

accompanying diagrammatic drawings in which:-

Figure 1 is a schematic circuit diagram of the pulsing arrangement for a single transmitting coil;

Figure 2 is a graph illustrating the voltage pulse applied to the coil of Figure 1 and the current in the coil produced by decaying eddy currents in a coin;

Figure 3 is an axial view of a large coil and showing the eddy currents induced in the periphery of a coin;

Figure 4 is a side elevation of a coin discriminating station utilising two coils of different sizes;

Figure 5 illustrates the eddy currents produced in coin by a voltage pulse of short duration in an adjacent coil;

Figure 6 is similar to Figure 5 but shows on a different scale the eddy currents produced by a long voltage pulses;

Figure 7 is a block circuit diagram of a single coil arrangement in which the coil is pulsed with a series of voltage pulses of different durations;

Figure 8 is a composite graph of applied voltage and coil current for the arrangement of Figure 7; and

Figure 9 is a front elevation of a coin validator in accordance with the invention.

Figures 1 and 2 are provided to explain the effects produced by pulsing a coil which is positioned with one end adjacent to the face of a coin. With reference to Figure 1, the resistive and inductive components of the coil are represented by R and L respectively. The coil is connected between ground and a V supply through a switch S, which in practice would be a suitable electronic circuit. The switch S, could be operated in response to detection of the presence of a coin at a coin testing station, but preferably it is operated by a pulse train of suitable repetition frequency to ensure that with moving coins at least one pulsing of the coil takes place with the coin adjacent to the coil.

In the arrangement of Figure 1 the same coil is used both as a 'transmitter' and 'receiver' in that the eddy currents induced in a coin by pulsing of the coil are monitored by detecting currents in the coil which result from the eddy currents, but as previously stated independent transmitting and receiving coils could be used.

The switch S of Figure 1 may be a VMOS transistor, such as IFR833 made by International Rectifier. This transistor is turned on by a pulse of preset length produced by a suitable electronic circuit. Such pulses may be initiated by the coin, by a coin feed mechanism, or a continuously operating pulse generator may be employed.

The currents in the coil L are monitored by a suitable monitoring circuit M connected through an amplifier A, and the stray capacitances of the coil and amplifier input are indicated as C. The input resistance of the amplifier A is arranged such that the coil L is critically damped. Closing of the switch S for a period of a few μ s produces a negative square voltage pulse in the coil, shown in Figure 2(b). The resulting current in the coil is

shown in Figure 2(a). The coil current increases in the negative direction during the presence of the voltage pulse, then reverses on termination of the voltage pulse, followed by an exponential curve $ke^{-t/\lambda}$ corresponding to the critically damped decay of current in the coil. Figure 2 shows that when a coin is present the eddy currents induced in the coin by the trailing edge of the voltage pulse and the associated induced currents in the coil decay at a slower rate which is monitored by circuit M by measuring the coil current at three predetermined times t_1 , t_2 and t_3 from the trailing edge of the voltage pulse.

The time constant λ of the exponential curve is proportional to the ratio L_1/R_1 where L_1 is the inductance of the short circuit turn provided by the coin and R_1 is the resistance of that turn.

In practice the time constant λ will not usually be computed. Instead it is preferred to compare the actual measurements of coil current at times t_1 , t_2 , t_3 with stored reference values or ranges. The stored values or ranges are conveniently stored in an EEPROM.

Figure 3 shows that the Induced currents in a coin 1 flow around the coin periphery '1' when the coin is placed adjacent to one end of a coil 2 which is of a diameter greater than that of the coin and where the projected area of the coil covers the coin. It will be understood that in this case L_1 is proportional to the area of the coin face, and R_1 to the coin radius. The ratio L_1/R_1 is therefore proportional to coin radius for a given type of coin material.

Figure 4 shows a coin discriminating station in accordance with the invention, and comprising large and small diameter coils 3 and 4 respectively positioned with their axes substantially parallel and with their adjacent ends closely spaced from one side of a coin path. The coins may slide along the coin path, but in this case the coins 6 are rolled along a plastics coin track 5. The larger coil 3 is of a diameter such that its projected areas will cover all of the range of coins which pass along track 5. The smaller coil 4 is of a diameter such that its projected area falls within the face of any coin within the range when it is positioned substantially centrally of the station as shown. The coils 3 and 4 are arranged to be pulsed independently and in sequence. The location of both coils 3 and 4 on the same side of the coin path and superimposed enables the larger coil 3 to be used as the receiver coil both for when that coil 3 is pulsed and also when the small coil is 4 is pulsed. Due to the geometry, the larger coil 3 will have a good flux linkage with the eddy current loop induced in the coin by the smaller coil 4, and is thereby most suited to act as a receiver coil when coil 4 is pulsed. This considerably simplifies the device since only one receiver section of the circuit is required to analyse the eddy currents as detected by the larger coil 3, and the number of coils is kept to a minimum.

Another advantage of positioning the coils on the same side of the coin path is that the opposite

side of the coin path may be left open, thereby minimising the chances of a coin jam.

The decaying eddy currents in the coins are monitored by a suitable monitoring circuit connected to coil 3 which in both cases compares the measurements of the current level at times t_1 , t_2 and t_3 . Figure 2, with respective stored values or ranges. Thus a single coin will give two sets of values of coil current for a pulse of a specified length, a first set of three corresponding to eddy currents flowing in the periphery of the coin, and a further set of three coil currents corresponding to eddy currents flowing in a short-circuit turn of diameter substantially equal to that of the smaller coil 4. As is explained in more detail hereafter with reference to Figures 5 and 6, one or more further sets of values are obtained by using pulses of different length.

The two sets of current values, corresponding to pulsing of coils 3 and 4 with pulses of the same length, are compared by suitable circuits with stored values of coil current which preferably are derived from actual measurements by the testing apparatus on sample coins, in order to determine the nature of the coin under test. It will be appreciated that since the time constant associated with the pulsing of smaller coil 4 does not depend upon coin size, whereas that associated with the pulsing of coil 3 is dependent on size, two sets of measurements enable many denominations of coin to be distinguished from each other without the need for additional tests to be performed.

Additional information about a coin may be obtained by measuring the coil current at more than three times, since although the eddy current decay curve is approximately exponential, it is not precisely so in all cases, due to the fact that the distribution of the decaying eddy currents in the coin varies with time. The eddy currents tend to penetrate to greater depths of the coin at later times, so that plated coins may be more easily identified by making current measurements over a more extended range of the eddy current decay curve.

Figure 5(a) and 5(b) correspond to the curves of Figures 2(a) and (b) respectively when a 5µs voltage pulse is applied to a coil, and the shading in Figures 5(c) and (d) illustrates how the induced eddy currents in a coin flow in the periphery of the coin for pulsing of a large diameter coil, and in the surface material of the coin face for a small diameter coil. Figures 6(a) to (d) similarly show what happens when a relatively long pulse is applied to a coil, 200µs, in this case. With a large coil, Figure 6(c), the eddy currents flow in a radially thick marginal portion of the coin, and with a small coil, Figure 6(d), the eddy currents flow in a loop which extends through the full thickness of the coin.

Plated coins, as used in many countries, will show different eddy current characteristics in dependence upon the depth to which the eddy currents penetrate, and so measurements of the decaying coil current for different lengths of pulse

enable plated coins to be distinguished from non-plated coins. Also, the resistance of the eddy current loop for long pulses will depend upon the thickness of the coin where the conditions are such that eddy currents would be produced through the full thickness of even a very thick coin, and such measurements may therefore be employed to determine the thickness of coins being tested.

Thus, it is arranged that one or both of the coil 3, 4 of the apparatus of Figure 4 is pulsed successively with pulses of different lengths to detect plated coins and to measure coin thickness, in addition to coin material and diameter. Again, the measured values of time constant are preferably compared with previously recorded values for sample coins. Since the electronics can work extremely quickly it is quite feasible to carry out all of these tests at one station using two coils only whilst the coins are moving quickly through the station.

In one embodiment of the invention, not shown, the coils 3, 4 are used in conjunction with a coin sorter of the inclined disc type. An inclined disc provided with marginal recesses picks out coins one by one from a hopper. The coils are positioned at a fixed location adjacent to the path of the disc recesses and prior to a series of exit gates provided with suitable means for removing the coins from the disc recesses. The exit gates are controlled in response to the output of the monitoring circuit to sort the coins. The disc is made of a plastics material so as not to influence the eddy current production.

Figure 7 is a block diagram of an embodiment of the invention which employs only a single coil 3 for both transmitting and receiving, and in which the coil is subject to a series of four voltage pulses of different lengths for each coin 6. The timing of the voltage pulses and the timing of the sampling of the coil current is controlled by a control unit U which contains suitable software for this purpose. The pulse and sampling sequence for the arrangement of Figure 7 is shown in Figure 8 which is a composite graph showing both the voltage pulses, as the negative ordinate, and the coil current, as the positive ordinate, against time t . At time t_a a negative going voltage is applied to the coil 3 by a pulse energisation circuit P and the pulse is terminated after 10µs at time t_b . The termination of the pulse gives rise, as in the previous arrangements described, to eddy currents in the coin which in turn produce a decaying current in the coil 3, shown as a dotted line in Figure 8. The coil current in the absence of a coin is also shown as a full line. The clipped top SAT results from saturation of the amplifier A connected between the coil 3 and the monitoring circuit. The control unit 3 provides a timing signal to the monitor M to effect sampling of the coil current by the monitor M at a time t_c which is 200µs after t_a . A sufficient length of time is then allowed to pass for the coil current to have decayed substantially to zero before a second, longer voltage pulse is initiated at time t_0 .

The second pulse lasts for 30 μ s and is terminated at time t_6 . Since a larger coil current has built up during the 30 μ s voltage pulse than for the 10 μ s pulse, the eddy currents produced in the coin on termination of the second pulse are greater than those for the first pulse, and accordingly the eddy currents decay more slowly. In accordance with a preferable feature of the invention the delay between the end of the second pulse and the time, at which the coil current is sampled is made greater, 30 μ s, then the corresponding delay t_6 to t_7 , 2 μ s, for the first pulse, in order to arrange that the coil current measured is within the dynamic range of the amplifier A and monitoring circuit M. This avoids the need for independent sampling circuits for the different pulses.

Similarly, third and fourth pulses of yet greater lengths 70 μ s and 120 μ s respectively are applied in succession to the coil 3 and sampling of the coil current takes place at times t_3 and t_4 respectively after delays of 40 μ s and 70 μ s respectively. Thus with this arrangement four values of coil current will be obtained for each coil from the measurements at times t_1 , t_2 , t_3 and t_4 and these four values are compared in Unit U with stored reference values or ranges to determine the denomination of the coin, or whether it is not acceptable.

It will be appreciated that it would be possible to use more or less than four pulses of different lengths as necessary to obtain the required degree of discrimination. It will also be appreciated that the order of pulsing does not have to be as shown in Figure 8.

In Figure 7 the size of coil 3 has been chosen to be greater than the diameter of all of the coins to be measured, but useful measurements could be made if the coil were to be as in Figure 5(d) and 6(d).

In view of the relatively short times of the pulses and sampling periods it is quite possible to use the arrangement of Figures 7 and 8 to make measurements on coins as they roll freely down the inclined coin path of a coin testing mechanism, all four measurement being carried out whilst the coin 6 is within the projected area of the coil 3.

A typical validator is shown schematically in Figure 9 and comprises an inclined moulded plastics plate 7 in the upper face, the front face in the drawing, of which is provided a channel 8 defining a coin path down which coins slide/roll when inserted into a coin slot 9. Coil 3 and a further check coil 10 are encapsulated within the plate 7, just below the surface of the base of channel 8. The amplifier A, monitor M and control unit U may conveniently be mounted on a circuit board secured to the rear of plate 7.

The check coil 10 is arranged to carry out similar measurements to the principal measuring coil 3, and its purpose is to check that a coin measured by coil 3 actually reaches the lower part of the mechanism, in order to counter fraudulent use in which coins attached to strings are withdrawn from the mechanism.

It will be appreciated that the validator arrange-

ment of Figure 9 may be arranged to operate in the manner of the Figure 4 arrangement by incorporating the further coil 4 within coil 3.

Since all the coils of the arrangement of Figure 9 are arranged within the moulded plate, the channel 8 can be left open thereby minimising the chances of a coin blockage.

Claims

1. A coin discriminating apparatus comprising coil means (3) for inducing eddy currents in a coin (6), pulsing means (S, U, P) for pulsing the coil means, and means (M) for monitoring the decay of eddy currents in the coin, characterised in that the pulsing means is arranged to pulse successively a coil or different coils of the coil means with voltage pulses of shorter and longer durations (t_1-t_2 , t_3-t_4).

2. A coin discriminating apparatus as claimed in claim 1 in which the delay (t_2-t_3 , t_4-t_5) between the lagging edge of a voltage pulse and the measurement of the eddy currents is longer for a longer voltage pulse than the corresponding delay for a shorter voltage pulse.

3. A coin discriminating apparatus as claimed in claim 1 or claim 2 in which the coil means comprises a single coil (3) only which is arranged to be pulsed successively with the pulses of different durations.

4. A coin discriminating apparatus as claimed in claim 1 or claim 2 in which first and second transmitting coils (3, 4) of the coil means are of larger and smaller effective cross-sectional areas respectively, the pulsing means is arranged to apply a voltage pulse to one of the transmitting coils followed by a voltage pulse to the other transmitting coil, and the monitoring means is arranged to monitor the decay of eddy currents produced in a coin by the lagging edge of the resulting current pulses in the transmitting coils when the coin is positioned adjacent to the respective transmitting coils.

5. A coin discriminating apparatus as claimed in claim 4 in which the projected effective cross-sectional area of the first transmitting coil onto a coin positioned adjacent to that coil by location means (5) is arranged to be greater than that of the face of at least most of the coins that are to be distinguished, the location means is so arranged that the boundary of said projected area of the first transmitting coil encircles the coin when the eddy currents are induced in the coin by pulsing of the first transmitting coil, and the arrangement is such that the projected effective cross-sectional area of the second transmitting coil lies within the area of the face of at least most of the coins when the coin is positioned adjacent to the second transmitting coil by the location means and that coil is pulsed.

6. A coin discriminating apparatus as claimed in claim 4 or claim 5 in which the first and second transmitting coils are positioned such that the coin being tested is substantially in the same position during pulsing of the first and second transmitting coils.

7. A coin discriminating apparatus as claimed in claim 4 or claim 5 in which the transmitting coils are placed at spaced positions along a coin path.

8. A coin discriminating apparatus as claimed in any of the claims 4 to 7 in which one or more of the coils of the coil means also acts as a receiver coil responsive to the induced eddy currents and is connected to the monitoring circuit.

9. A coin discriminating apparatus as claimed in claim 8 as appended to claim 6 in which the first and second transmitting coils are positioned together, and the first transmitting coil acts as the receiver coil both for when the first transmitting coil is pulsed and when the second transmitting coil is pulsed.

10. A coin discriminating apparatus as claimed in any of the preceding claims in which the monitoring circuit is arranged to measure the magnitude of the decaying eddy currents produced by each pulse of the coil means at at least three predetermined times (t_1 , t_2 , t_3) subsequent to the initiation of the eddy currents.

Patentansprüche

1. Münzenerkennungsvorrichtung mit einer Spulenordnung (3), mittels deren in einer Münze (6) Wirbelströme erzeugbar sind, mit einem Impulserzeuger (S, U, P), mittels dessen die Spulenordnung mit Impulsen beaufschlagbar ist, und mit einer Einrichtung (M), mittels deren der Abfall der Wirbelströme in der Münze erfassbar ist, dadurch gekennzeichnet, daß mittels des Impulserzeugers eine Spule oder verschiedene Spulen der Spulenordnung nacheinander mit Spannungsimpulsen kürzerer und längerer Dauer ($t_A - t_B$, $t_C - t_D$) beaufschlagbar sind.

2. Münzenerkennungsvorrichtung nach Anspruch 1, bei der die Verzögerung ($t_B - t_C$, $t_D - t_E$) zwischen dem Ende eines Spannungsimpulses und der Messung der Wirbelströme bei einem längeren Spannungsimpuls länger als die entsprechende Verzögerung bei einem kürzeren Spannungsimpuls ist.

3. Münzenerkennungsvorrichtung nach Anspruch 1 oder 2, bei der die Spulenordnung nur eine einzige Spule (3) umfaßt, die nacheinander mit Impulsen unterschiedlicher Dauer beaufschlagbar ist.

4. Münzenerkennungsvorrichtung nach Anspruch 1 oder 2, bei der eine erste und eine zweite Übertragungsspule (3, 4) der Spulenordnung einen größeren bzw. einen kleineren wirksamen Querschnitt besitzen, bei der mittels des Impulserzeugers ein Spannungsimpuls auf eine der Übertragungsspulen und im Anschluß daran ein Spannungsimpuls auf die andere Übertragungsspule aufgebbar sind und bei der mittels der Erfassungseinrichtung der Abfall der in einer Münze erzeugten Wirbelströme durch das Ende der resultierenden Stromimpulse in den Übertragungsspulen erfassbar ist, wenn sich die Münze in der Nähe der jeweiligen Übertragungsspule befindet.

5. Münzenerkennungsvorrichtung nach

Anspruch 4, bei welcher die auf eine Münze, die durch eine Positioniereinrichtung (5) in der Nähe einer ersten Übertragungsspule positioniert ist, projizierte wirksame Querschnittsfläche dieser Übertragungsspule größer als die Fläche mindestens der meisten zu unterscheidenden Münzen ist, bei welcher die Positioniereinrichtung so angeordnet ist, daß die Grenze der besagten projizierten Fläche der ersten Übertragungsspule die Münze umgibt, wenn durch impulsweise Beaufschlagung der ersten Übertragungsspule in der Münze die Wirbelströme erzeugt werden, und bei welcher die projizierte wirksame Querschnittsfläche der zweiten Übertragungsspule innerhalb der Fläche mindestens der meisten Münzen liegt, wenn die Münze durch die Positioniereinrichtung nahe an der zweiten Übertragungsspule positioniert und diese Spule beaufschlagt ist.

6. Münzenerkennungsvorrichtung nach Anspruch 4 oder 5, bei welcher die erste und die zweite Übertragungsspule so angeordnet sind, daß die zu prüfende Münze sich bei der impulsweisen Beaufschlagung der ersten und zweiten Übertragungsspule im wesentlichen in der gleichen position befindet.

7. Münzenerkennungsvorrichtung nach Anspruch 4 oder 5, bei welcher die Übertragungsspulen mit Längsabstand voneinander entlang einer Münzenbahn angeordnet sind.

8. Münzenerkennungsvorrichtung nach einem der Ansprüche 4 bis 7, bei welcher eine oder mehrere der Spulen der Spulenordnung auch als Empfängerspule wirkt, die auf die induzierten Wirbelströme anspricht, und mit dem Erfassungsschaltkreis verbunden ist.

9. Münzenerkennungsvorrichtung nach Anspruch 6 und 8, bei welcher die erste und die zweite Übertragungsspule beieinander angeordnet sind und die erste Übertragungsspule sowohl bei der Beaufschlagung der ersten Übertragungsspule als auch bei der Beaufschlagung der zweiten Übertragungsspule als Empfängerspule wirkt.

10. Münzenerkennungsvorrichtung nach einem der vorangehenden Ansprüche, bei welcher der Erfassungsschaltkreis die Größe der durch jeden Impuls der Spulenordnung hervorgerufenen abfallenden Wirbelströme in mindestens drei vorbestimmten Zeitpunkten (t_1 , t_2 , t_3) jeweils nach Hervorrufung der Wirbelströme mißt.

Revendications

1. Dispositif de discrimination de pièces de monnaie comprenant un moyen à enroulements (3) en vue d'induire des courants de Foucault dans une pièce de monnaie (6), un moyen pulseur (S, U, P) en vue de pulser le moyen à enroulements, ainsi qu'un moyen (M) en vue de contrôler l'évanouissement des courants de Foucault dans la pièce de monnaie, caractérisé en ce que le moyen pulseur est conçu pour pulser successivement un ou des enroulements différents du moyen à enroulements avec des impulsions de tension de durées plus courtes et plus longues ($t_A - t_B$, $t_C - t_D$).

2. Dispositif de discrimination de pièces de monnaie selon la revendication 1, caractérisé en ce que le retard ($t_0 - t_c$, $t_e - t_c$) entre le flanc postérieur d'une impulsion de tension et la mesure des courants de Foucault est plus long pour une impulsion de tension plus longue que le retard correspondant pour une impulsion de tension plus courte.

3. Dispositif de discrimination de pièces de monnaie selon la revendication 1 ou 2, caractérisé en ce que le moyen à enroulements comprend un seul enroulement (3) qui est conçu pour être pulsé successivement par les impulsions de durées différentes.

4. Dispositif de discrimination de pièces de monnaie selon la revendication 1 ou 2, dans lequel le premier et le second enroulement de transmission (3, 4) du moyen à enroulements ont respectivement des sections transversales efficaces plus grandes et plus petites, le moyen pulseur étant conçu pour appliquer une impulsion de tension à un des enroulements de transmission, suivie d'une impulsion de tension à l'autre enroulement de transmission, tandis que le moyen de contrôle est conçu pour contrôler l'évanouissement des courants de Foucault se produisant dans une pièce de monnaie par le flanc postérieur des impulsions de courant obtenues dans les enroulements de transmission lorsque la pièce de monnaie est située dans une position adjacente aux enroulements respectifs de transmission.

5. Dispositif de discrimination de pièces de monnaie selon la revendication 4, caractérisé en ce que la section transversale effective projetée du premier enroulement de transmission sur une pièce de monnaie située dans une position adjacente à cet enroulement par un moyen de localisation (5) est conçue pour être plus grande que celle de la face d'au moins la plupart des pièces de monnaie qui doivent être distinguées, le moyen de localisation étant conçu de telle sorte que les limites de la surface projetée du premier enroulement de transmission entourent la pièce de monnaie lors de l'induction des courants de Foucault dans cette dernière par impulsion du premier enroulement de transmission, le système

étant conçu de telle sorte que la section transversale effective projetée du deuxième enroulement de transmission se situe dans la zone de la face d'au moins la majeure partie des pièces de monnaie lorsque la pièce de monnaie est située dans une position adjacente au second enroulement de transmission par le moyen de localisation et que l'enroulement est pulsé.

6. Dispositif de discrimination de pièces de monnaie selon la revendication 4 ou 5, caractérisé en ce que le premier et le second enroulement de transmission sont localisés de telle sorte que la pièce de monnaie devant être soumise à l'essai occupe pratiquement la même position au cours de l'application d'impulsions au premier et au second enroulement de transmission.

7. Dispositif de discrimination de pièces de monnaie selon la revendication 4 ou 5, dans lequel les enroulements de transmission sont placés dans des positions espacées le long d'un parcours d'une pièce de monnaie.

8. Dispositif de discrimination de pièces de monnaie selon l'une quelconque des revendications 4 à 7, dans lequel un ou plusieurs des enroulements du moyen à enroulements agit ou agissent également comme enroulements récepteurs réagissant aux courants de Foucault induits, tandis qu'il(s) est ou sont raccordé(s) au circuit de contrôle.

9. Dispositif de discrimination de pièces de monnaie selon la revendication 8 en fonction de la revendication 6, caractérisé en ce que le premier et le second enroulement de transmission sont localisés ensemble, le premier enroulement de transmission faisant office d'enroulement récepteur à la fois lorsque le premier enroulement de transmission est pulsé et lorsque le second enroulement de transmission est également pulsé.

10. Dispositif de discrimination de pièces de monnaie selon l'une quelconque des revendications précédentes, dans lequel le circuit de contrôle est conçu pour mesurer l'amplitude des courants de Foucault s'évanouissant produits par chaque impulsion du moyen à enroulements au moins à trois moments prédéterminés (t_1 , t_2 , t_3) suite à l'armorage de ces courants de Foucault.

50

55

60

65

8

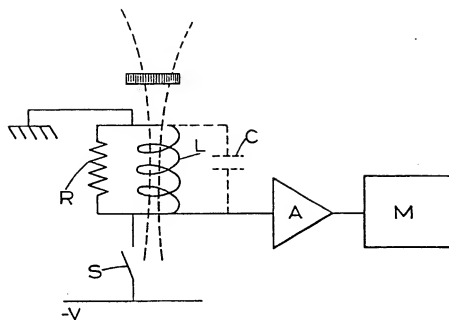
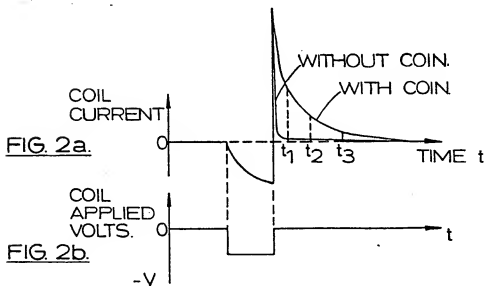


FIG. 1



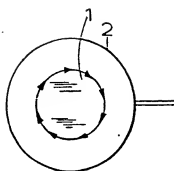


FIG. 3.

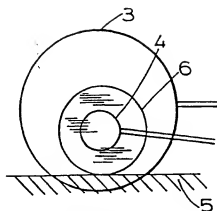


FIG. 4.

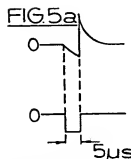


FIG. 5b

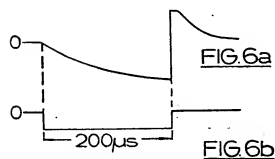


FIG. 6b

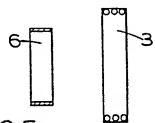


FIG. 5c

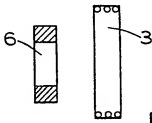


FIG. 6c

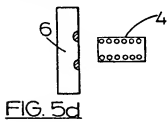


FIG. 5d

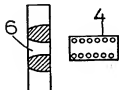


FIG. 6d

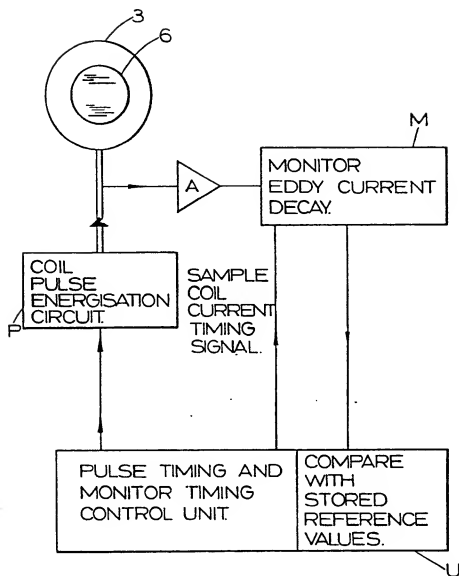


FIG. 7

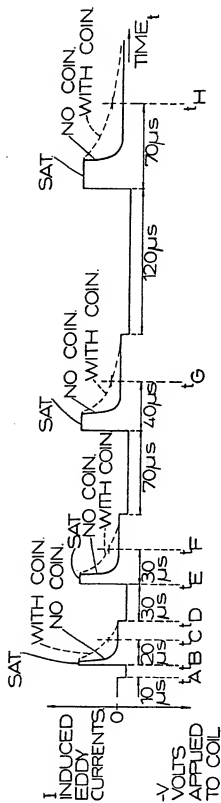


FIG. 8.

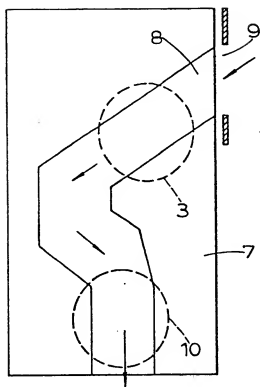


FIG. 9.